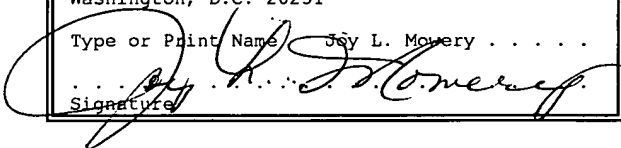


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SPEECH CODING WITH COMFORT NOISE VARIABILITY FEATURE
FOR INCREASED FIDELITY

This application claims the priority under 35 USC 119(e)(1) of copending U.S. Provisional Application No. 60/109,555, filed on November 23, 1998.

FIELD OF THE INVENTION

The invention relates generally to speech coding and, more particularly, to speech coding wherein artificial background noise is produced during periods of speech inactivity.

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BACKGROUND OF THE INVENTION

Speech coders and decoders are conventionally provided in radio transmitters and radio receivers, respectively, and are cooperable to permit speech communications between a given transmitter and receiver over a radio link. The combination of a speech coder and a speech decoder is often referred to as a speech codec. A mobile radiotelephone (e.g., a cellular telephone) is an example of a conventional communication device that typically includes a radio transmitter having a speech coder, and a radio receiver having a speech decoder.

In conventional block-based speech coders the incoming speech signal is divided into blocks called frames. For common 4kHz telephony bandwidth applications typical framelengths are 20ms or 160 samples. The frames are further divided into subframes, typically of length 5ms or 40 samples.

Conventional linear predictive analysis-by-synthesis (LPAS) coders use speech production related models. From the input speech signal, model parameters describing the vocal tract, pitch etc. are extracted. Parameters that vary slowly are typically computed for every frame.

Examples of such parameters include the STP (short term prediction) parameters that describe the vocal tract in the apparatus that produced the speech. One example of STP parameters is linear prediction coefficients (LPC) that represent the spectral shape of the input speech signal. Examples of parameters that vary more rapidly include the pitch and innovation shape/gain parameters, which are typically computed every subframe.

The extracted parameters are quantized using suitable well-known scalar and vector quantization techniques. The STP parameters, for example linear prediction coefficients, are often transformed to a representation more suited for quantization such as Line Spectral Frequencies (LSFs). After quantization, the parameters are transmitted over the communication channel to the decoder.

In a conventional LPAS decoder, generally the opposite of the above is done, and the speech signal is synthesized. Postfiltering techniques are usually applied to the synthesized speech signal to enhance the perceived quality.

For many common background noise types a much lower bit rate than is needed for speech provides a good enough model of the signal. Existing mobile systems make use of this fact by adjusting the transmitted bit rate accordingly during background noise. In conventional systems using continuous transmission techniques, a variable rate (VR) speech coder may use its lowest bit rate. In conventional Discontinuous Transmission (DTX) schemes, the transmitter stops sending coded speech frames when the speaker is inactive. At regular or irregular intervals (typically every 500 ms), the transmitter sends speech parameters suitable for generation of comfort noise in the decoder. These parameters for comfort noise generation (CNG) are conventionally coded into what is sometimes called Silence Descriptor (SID) frames. At the receiver, the decoder uses the comfort noise parameters received in the SID frames to synthesize artificial noise by means of a conventional comfort noise injection (CNI) algorithm.

When comfort noise is generated in the decoder in a conventional DTX system, the noise is often perceived as being very static and much different from the background

noise generated in active (non-DTX) mode. The reason for this perception is that DTX SID frames are not sent to the receiver as often as normal speech frames. In LPAS codecs having a DTX mode, the spectrum and energy of the background noise are typically estimated (for example, averaged) over several frames, and the estimated parameters are then quantized and transmitted over the channel to the decoder. FIGURE 1 illustrates an exemplary prior art comfort noise encoder that produces the aforementioned estimated background noise (comfort noise) parameters. The quantized comfort noise parameters are typically sent every 100 to 500ms.

The benefit of sending SID frames with a low update rate instead of sending regular speech frames is twofold. The battery life in, for example, a mobile radio transceiver, is extended due to lower power consumption, and the interference created by the transmitter is lowered thereby providing higher system capacity.

In a conventional decoder, the comfort noise parameters can be received and decoded as shown in FIGURE 2. Because the decoder does not receive new comfort noise parameters as often as it normally receives speech

parameters, the comfort noise parameters which are received in the SID frames are typically interpolated at 23 to provide a smooth evolution of the parameters in the comfort noise synthesis. In the synthesis operation, shown generally at 25, the decoder inputs to the synthesis filter 27 a gain scaled random noise (e.g., white noise) excitation and the interpolated spectrum parameters. As a result, the generated comfort noise $s_c(n)$, will be perceived as highly stationary ("static"), regardless of whether the background noise $s(n)$ at the encoder end (see FIGURE 1) is changing in character. This problem is more pronounced in backgrounds with strong variability, such as street noise and babble (e.g., restaurant noise), but is also present in car noise situations.

One conventional approach to solving this "static" comfort noise problem is simply to increase the update rate of DTX comfort noise parameters (e.g., use a higher SID frame rate). Exemplary problems with this solution are that battery consumption (e.g., in a mobile transceiver) will increase because the transmitter must be operated more often, and system capacity will decrease

because of the increased SID frame rate. Thus, it is common in conventional systems to accept the static background noise.

5 It is therefore desirable to avoid the
aforementioned disadvantages associated with conventional
comfort noise generation.

According to the invention, conventionally generated
comfort noise parameters are modified based on properties
of actual background noise experienced at the encoder.
10 Comfort noise generated from the modified parameters is
perceived as less static than conventionally generated
comfort noise, and more similar to the actual background
noise experienced at the encoder.

BRIEF DESCRIPTION OF THE DRAWINGS

FIGURE 1 diagrammatically illustrates the production of comfort noise parameters in a conventional speech encoder.

5 FIGURE 2 diagrammatically illustrates the generation of comfort noise in a conventional speech decoder.

FIGURE 3 illustrates a comfort noise parameter modifier for use in generating comfort noise according to the invention.

10 FIGURE 4 illustrates an exemplary embodiment of the modifier of FIGURE 3.

FIGURE 5 illustrates an exemplary embodiment of the variability estimator of FIGURE 4.

15 FIGURE 5A illustrates exemplary control of the SELECT signal of FIGURE 5.

FIGURE 6 illustrates an exemplary embodiment of the modifier of FIGURES 3-5, wherein the variability estimator of FIGURE 5 is provided partially in the encoder and partially in the decoder.

20 FIGURE 7 illustrates exemplary operations which can be performed by the modifier of FIGURES 3-6.

FIGURE 8 illustrates an example of the estimating step of FIGURE 7.

FIGURE 9 illustrates a voice communication system in which the modifier embodiments of FIGURES 3-8 can be implemented.

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DETAILED DESCRIPTION

FIGURE 3 illustrates a comfort noise parameter modifier 30 for modifying comfort noise parameters according to the invention. In the example of FIGURE 3, the modifier 30 receives at an input 33 the conventional interpolated comfort noise parameters, for example the spectrum and energy parameters output from interpolator 23 of FIGURE 2. The modifier 30 also receives at input 31 spectrum and energy parameters associated with background noise experienced at the encoder. The modifier 30 modifies the received comfort noise parameters based on the background noise parameters received at 31 to produce modified comfort noise parameters at 35. The modified comfort noise parameters can then be provided, for example, to the comfort noise synthesis section 25 of FIGURE 2 for use in conventional comfort noise synthesis operations. The modified comfort noise parameters provided at 35 permit the synthesis section 25 to generate comfort noise that reproduces more faithfully the actual background noise presented to the speech encoder.

FIGURE 4 illustrates an exemplary embodiment of the comfort noise parameter modifier 30 of FIGURE 3. The modifier 30 includes a variability estimator 41 coupled to input 31 in order to receive the spectrum and energy parameters of the background noise. The variability estimator 41 estimates variability characteristics of the background noise parameters, and outputs at 43 information indicative of the variability of the background noise parameters. The variability information can characterize the variability of the parameter about the mean value thereof, for example the variance of the parameter, or the maximum deviation of the parameter from the mean value thereof.

The variability information at 43 can also be indicative of correlation properties, the evolution of the parameter over time, or other measures of the variability of the parameter over time. Examples of time variability information include simple measures such as the rate of change of the parameter (fast or slow changes), the variance of the parameter, the maximum deviation of the mean, other statistical measures characterizing the variability of the parameter, and more

advanced measures such as autocorrelation properties, and filter coefficients of an auto-regressive (AR) predictor estimated from the parameter. One example of a simple rate of change measure is counting the zero crossing
5 rate, that is, the number of times that the sign of the parameter changes when looking from the first parameter value to the last parameter value in the sequence of parameter values. The information output at 43 from the estimator 41 is input to a combiner 45 which combines the
10 output information at 43 with the interpolated comfort noise parameters received at 33 in order to produce the modified comfort noise parameters at 35.

FIGURE 5 illustrates an exemplary embodiment of the variability estimator 41 of FIGURE 4. The estimator of
15 FIGURE 5 includes a mean variability determiner 51 coupled to input 31 for receiving the spectrum and energy parameters of the background noise. The mean variability determiner 51 can determine mean variability characteristics as described above. For example, if the
20 background noise buffer 37 of FIGURE 3 includes 8 frames and 32 subframes, then the variability of the buffered spectrum and energy parameters can be analyzed as

follows. The mean (or average) value of the buffered spectrum parameters can be computed (as is conventionally done in DTX encoders to produce SID frames) and subtracted from the buffered spectrum parameter values, thereby yielding a vector of spectral deviation values. Similarly, the mean subframe value of the buffered energy parameters can be computed (as is conventionally done in DTX encoders to produce SID frames), and then subtracted from the buffered subframe energy parameter values, thereby yielding a vector of energy deviation values. The spectrum and energy deviation vectors thus comprise mean-removed values of the spectrum and energy parameters. The spectrum and energy deviation vectors are communicated from the variability determiner 51 to a deviation vector storage unit 55 via a communication path 52.

A coefficient calculator 53 is also coupled to the input 31 in order to receive the background noise parameters. The exemplary coefficient calculator 53 is operable to perform conventional AR estimations on the respective spectrum and energy parameters. The filter coefficients resulting from the AR estimations are

communicated from the coefficient calculator 53 to a filter 57 via a communication path 54. The filter coefficients calculated at 53 can define, for example, respective all-pole filters for the spectrum and energy parameters.

In one embodiment, the coefficient calculator 53 performs first order AR estimations for both the spectrum and energy parameters, calculating filter coefficients $a_1 = R_{xx}(1)/R_{xx}(0)$ for each parameter in conventional fashion. $R_{xx}(0)$ and $R_{xx}(1)$ values are conventional autocorrelation values of the particular parameter:

$$R_{xx}(0) = \sum_{n=0}^{N-1} x(n) * x(n)$$

$$R_{xx}(1) = \sum_{n=0}^{N-1} x(n) * x(n-1)$$

In these R_{xx} calculations, x represents the background noise (e.g., spectrum or energy) parameter. A positive value of a_1 generally indicates that the parameter is varying slowly, and a negative value generally indicates rapid variation.

According to one embodiment, for each frame of the spectrum parameters, and for each subframe of the energy parameters, a component $x(k)$ from the corresponding deviation vector can be, for example, randomly selected
5 (via a SELECT input of storage unit 55) and filtered by the filter 57 using the corresponding filter coefficients. The output from the filter is then scaled by a constant scale factor via a scaling apparatus 59, for example a multiplier. The scaled output, designated
10 as $x_p(k)$ in FIGURE 5, is provided to the input 43 of the combiner 45 of FIGURE 4.

In one embodiment, illustrated diagrammatically in FIGURE 5A, a zero crossing rate determiner 50 is coupled at 31 to receive the buffered parameters at 37. The
15 determiner 50 determines the respective zero crossing rates of the spectrum and energy parameters. That is, for the sequence of energy parameters buffered at 37, and also for the sequence of spectrum parameters buffered at 37, the zero crossing rate determiner 50 determines the
20 number of times in the respective sequence that the sign of the associated parameter value changes when looking from the first parameter value to the last parameter

value in the buffered sequence. This zero crossing rate information can then be used at 56 to control the SELECT signal of FIGURE 5.

For example, for a given deviation vector, the
5 SELECT signal can be controlled to randomly select components $x(k)$ of the deviation vector relatively more frequently (as often as every frame or subframe) if the zero crossing rate associated with that parameter is relatively high (indicating relatively high parameter
10 variability), and to randomly select components $x(k)$ of the deviation vector relatively less frequently (e.g., less often than every frame or subframe) if the associated zero crossing rate is relatively low (indicating relatively low parameter variability). In
15 other embodiments, the frequency of selection of the components $x(k)$ of a given deviation vector can be set to a predetermined, desired value.

The combiner of FIGURE 4 operates to combine the scaled output $x_p(k)$ with the conventional comfort noise
20 parameters. The combining is performed on a frame basis for spectral parameters, and on a subframe basis for energy parameters. In one example, the combiner 45 can

be an adder that simply adds the signal $x_p(k)$ to the conventional comfort noise parameters. The scaled output $x_p(k)$ of FIGURE 5 can thus be considered to be a perturbing signal which is used by the combiner 45 to perturb the conventional comfort noise parameters received at 33 in order to produce the modified (or perturbed) comfort noise parameters to be input to the comfort noise synthesis section 25 (see FIGURES 2-4).

The conventional comfort noise synthesis section 25 can use the perturbed comfort noise parameters in conventional fashion. Due to the perturbation of the conventional parameters, the comfort noise produced will have a semi-random variability that significantly enhances the perceived quality for more variable backgrounds such as babble and street noise, as well as for car noise.

The perturbing signal $x_p(k)$ can, in one example, be expressed as follows:

$$x_p(k) = \beta_x \cdot (b_{0x} \cdot x(k) - a_{1x} \cdot \gamma_x \cdot (x_p(k-1))),$$

where β_x is a scaling factor, b_{0x} and a_{1x} are filter coefficients, and γ_x is a bandwidth expansion factor.

The broken line in FIGURE 5 illustrates an embodiment wherein the filtering operation is omitted, and the perturbing signal $x_p(k)$ comprises scaled deviation vector components.

5 In some embodiments, the modifier 30 of FIGURES 3-5 is provided entirely within the speech decoder (see FIGURE 9), and in other embodiments the modifier of FIGURES 3-5 is distributed between the speech encoder and the speech decoder (see broken lines in FIGURE 9). In
10 embodiments where the modifier 30 is provided entirely in the decoder, the background noise parameters shown in FIGURE 3 must be identified as such in the decoder. This can be accomplished by buffering at 37 a desired amount (frames and subframes) of the spectrum and energy
15 parameters received from the encoder via the transmission channel. In a DTX scheme, implicit information conventionally available in the decoder can be used to decide when the buffer 37 contains only parameters associated with background noise. For example, if the
20 buffer 37 can buffer N frames, and if N frames of hangover are used after speech segments before the transmission is interrupted for DTX mode (as is

conventional), then these last N frames before the switch to DTX mode are known to contain spectrum and energy parameters of background noise only. These background noise parameters can then be used by the modifier 30 as described above.

In embodiments where the modifier 30 is distributed between the encoder and the decoder, the mean variability determiner 51 and the coefficient calculator 53 can be provided in the encoder. Thus, the communication paths 52 and 54 in such embodiments are analogous to the conventional communication path used to transmit conventional comfort noise parameters from encoder to decoder (see FIGURES 1 and 2). More particularly, as shown in example FIGURE 6, the paths 52 and 54 proceed through a quantizer (see also FIGURE 1), a communication channel (see also FIGURES 1 and 2) and an unquantizing section (see also FIGURE 2) to the storage unit 55 and the filter 57, respectively (see also FIGURE 5). Well known techniques for quantization of scalar values as well as AR filter coefficients can be used with respect to the mean variability and AR filter coefficient information.

5 The encoder knows, by conventional means, when the spectrum and energy parameters of background noise are available for processing by the mean variability determiner 51 and the coefficient calculator 53, because these same spectrum and energy parameters are used conventionally by the encoder to produce conventional comfort noise parameters. Conventional encoders typically calculate an average energy and average spectrum over a number of frames, and these average spectrum and energy parameters are transmitted to the decoder as comfort noise parameters. Because the filter coefficients from coefficient calculator 53 and the deviation vectors from mean variability determiner 51 must be transmitted from the encoder to the decoder across the transmission channel as shown in FIGURE 6, extra bandwidth is required when the modifier is distributed between the encoder and the decoder. In contrast, when the modifier is provided entirely in the decoder, no extra bandwidth is required for its implementation.

FIGURE 7 illustrates the above-described exemplary operations which can be performed by the modifier

embodiments of FIGURES 3-5. It is first determined at 71 whether the available spectrum and energy parameters (e.g., in buffer 37 of FIGURE 3) are associated with speech or background noise. If the available parameters are associated with background noise, then properties of the background noise, such as mean variability and time variability are estimated at 73. Thereafter at 75, the interpolated comfort noise parameters are perturbed according to the estimated properties of the background noise. The perturbing process at 75 is continued as long as background noise is detected at 77. If speech activity is detected at 77, then availability of further background noise parameters is awaited at 71.

FIGURE 8 illustrates exemplary operations which can be performed during the estimating step 73 of FIGURE 7. The processing considers N frames and kN subframes at 81, corresponding to the aforementioned N buffered frames. In one embodiment, $N=8$ and $k=4$. A vector of spectrum deviations having N components is obtained at 83 and a vector of energy deviations having kn components is obtained at 85. At 87, a component is selected (for example, randomly) from each of the deviation vectors.

At 89, filter coefficients are calculated, and the selected vector components are filtered accordingly. At 88, the filtered vector components are scaled in order to produce the perturbing signal that is used at step 75 in
5 FIGURE 7. The broken line in FIGURE 8 corresponds to the broken line embodiments of FIGURE 5, namely the embodiments wherein the filtering is omitted and scaled deviation vector components are used as the perturbing parameters.

10 FIGURE 9 illustrates an exemplary voice communication system in which the comfort noise parameter modifier embodiments of FIGURES 3-8 can be implemented. A transmitter XMTR includes a speech encoder 91 which is coupled to a speech decoder 93 in a receiver RCVR via a
15 transmission channel 95. One or both of the transmitter and receiver of FIGURE 9 can be part of, for example, a radiotelephone, or other component of a radio communication system. The channel 95 can include, for example, a radio communication channel. As shown in
20 FIGURE 9, the modifier embodiments of FIGURES 3-8 can be implemented in the decoder, or can be distributed between

the encoder and the decoder (see broken lines) as described above with respect to FIGURES 5 and 6.

It will be evident to workers in the art that the embodiments of FIGURES 3-9 above can be readily
5 implemented, for example, by suitable modifications in software, hardware, or both, in conventional speech codecs.

The invention described above improves the naturalness of background noise (with no additional
10 bandwidth or power cost in some embodiments). This makes switching between speech and non-speech modes in a speech codec more seamless and therefore more acceptable for the human ear.

Although exemplary embodiments of the present
15 invention have been described above in detail, this does not limit the scope of the invention, which can be practiced in a variety of embodiments.